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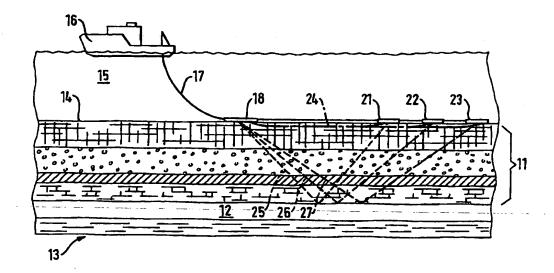
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(54) Title: METHOD AND APPARATUS FOR DETERMINING THE NATURE OF SUBTERRANEAN RESERVOIRS



(57) Abstract

A system for determining the nature of a subterranean reservoir (12) whose position and geometry is known from previous seismic surveys. An electromagnetic field (24, 25, 26, 27) is applied by a transmitter (18) on the seabed (14) and detected by antennea (21, 22, 23) also on the seabed (14). The nature of the detected reflected waves (25, 26, 27) is used to determine whether the reservoir (12) contains water or hydrocarbons.

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Method and Apparatus for Determining the Nature of Subterranean Reservoirs

The present invention relates to a method and apparatus for determining the nature of submarine and subterranean reservoirs. More particularly, the invention is concerned with determining whether a reservoir, whose approximate geometry and location are known, contains hydrocarbons or water.

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Currently, the most widely used techniques for geological surveying, particularly in sub-marine situations, are seismic methods. These seismic techniques are capable of revealing the structure of the subterranean strata with some accuracy. However, whereas a seismic survey can reveal the location and shape of a potential reservoir, it cannot reveal the nature of the reservoir.

The solution therefore is to drill a borehole into the reservoir. However, the costs involved in drilling an exploration well tend to be in the region of £25m and since the success rate is generally about 1 in 10, this tends to be a very costly exercise.

It is therefore an object of the invention to provide a system for determining, with greater certainty, the nature of a subterranean reservoir without the need to sink a borehole.

According to one aspect of the invention, there is provided a method of determining the nature of a subterranean reservoir whose approximate geometry and location are known, which comprises: applying a time varying electromagnetic field to the strata containing the reservoir; detecting the electromagnetic wave field response; and analysing the effects on the characteristics of the detected field that have been caused by the reservoir, thereby determining the content of the

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reservoir, based on the analysis.

According to another aspect of the invention, there is provided apparatus for determining the nature of a subterranean reservoir whose approximate geometry and location are known comprising: means for applying a time varying electromagnetic field to the strata containing the reservoir; means for detecting the electromagnetic wave field response, and means for analysing the effects on the detected field that have been caused by the reservoir, thereby enabling the content of the reservoir to be determined based on the analysis.

It has been appreciated by the present applicants that while the seismic properties of oil-filled strata and water-filled strata do not differ significantly, their electromagnetic resistivities/ permittivities do differ. Thus, by using an electromagnetic surveying method, these differences can be exploited and the success rate in predicting the nature of a reservoir can be increased significantly. This represents potentially an enormous cost saving.

The technique is applicable in exploring land-based subterranean reservoirs but is especially applicable to submarine, in particular sub-sea, subterranean reservoirs. Preferably the field is applied using one or more stationary transmitters located on the earth's surface, and the detection is carried out by one or more stationary receivers located on the earth's surface. In a preferred application, the transmitter(s) and/or receivers are located on or close to the seabed or the bed of some other area of water. Conveniently, there will be a single transmitter and an array of receivers, the transmitter(s) and receivers being dipole antennae or coils, though other forms of transmitter/receivers can be used. Also, if improved directionality of the emitted field is desirable,

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then a plurality of transmitters with phase adjustment can be used.

Electromagnetic surveying techniques in themselves are known. However, they are not widely used in practice. In general, the reservoirs of interest are about 1 km or more below the sea bed. In order to carry out electromagnetic surveying in these conditions, with any reasonable degree of resolution, short wavelengths are necessary. Unfortunately, such short wavelengths suffer from very high attenuation. Long wavelengths do not provide adequate resolution. For these reasons, seismic techniques are preferred.

However, while longer wavelengths applied by electromagnetic techniques cannot provide sufficient information to provide an accurate indication of the boundaries of the various strata, if the geological structure is already known, they can be used to determine the nature of a particular identified formation, if the possibilities for the nature of that formation have significantly differing electromagnetic characteristics. The resolution is not particularly important and so longer wavelengths which do not suffer from excessive attenuation can be employed.

The resistivity of sea water is about 0.3 ohm-m and that of the overburden beneath the sea bed would typically be from 0.3 to 4 ohm-m, for example about 2 ohm-m. However, the resisitivty of an oil reservoir is likely to be about 50 ohm-m. This large difference can be exploited using the techniques of the present invention. Typically, the resisitivity of a hydrocarbon-bearing formation will be 20 to 400 times greater than water-bearing formation.

Due to the different electromagnetic properties of a gas/oil bearing formation and a water bearing formation,

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one can expect a reflection of the transmitted field at the boundary of a gas/oil bearing formation. However, the similarity between the properties of the overburden and a reservoir containing water means that no reflection is likely to occur.

The transmitted field may be pulsed, however, a coherent continuous wave with stepped frequencies is preferred. It may be transmitted for a significant period of time, during which the transmitter should preferably be stationary, and the transmission stable. Thus, the field may be transmitted for a period of time from 30 seconds to 60 minutes, preferably from 3 to 30 minutes, for example about 20 minutes. Preferably, the receivers are arranged to detect a direct wave and a wave reflected from the reservoir, and the analysis includes extraacting phase and amplitude data of the reflected wave from corresponding data from the direct wave.

The direct wave, which progresses via the sea water and the surface layers of the overburden, will reach the receivers first and will be much stronger than the later reflected waves. In an alternative system, therefore, the direct wave may be suppressed, using known techniques. This means that the receivers used will not require such a large dynamic range.

Preferably, the wavelength of the transmission is given by the formula

$0.1s \le \lambda \le 10s$;

where λ is the wavelength of the transmission through the overburden and s is the distance from the seabed to the reservoir. More preferably λ is from about 0.5s to 2s. This may be achieved by adopting a transmission frequency

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from 0.1 Hz to 1 kHz, preferably from 1 to 50 Hz, for example 20 Hz.

In a preferred regime, a first transmission is made at a first frequency and received by each receiver in a tuned array of receivers, then a second transmission is made at a second frequency and received by the same tuned array of receivers, the receivers being tuned to receive their respective transmission. This would probably be repeated several more times, though it may only be carried out once.

Preferably, the analysis includes comparing the results of the measurements taken with the results of a mathematical simulation model based on the known properties of the reservoir and overburden conditions.

Preferably, the distance between the transmitter and a receiver is given by the formula

$0.5 \lambda \leq 1 \leq 10 \lambda$;

where λ is the wavelength of the transmission through the overburden and 1 is the distance between the transmitter and the first receiver.

Given that the distance s and the geometry of the reservoir will be known from previous seismic surveys, an optimum λ and 1 would be selected.

Where dipole antennae are used these may be fixed, however, they are preferably adapted antennae which can be tuned for optimum transmission and reception in dependence upon the frequency of the transmission and its wavelength—through the overburden. This may be achieved by altering—their effective length either by remote controlled relays or by electronic switching systems. In addition, the driving circuit may be tuned in order to increase the

bandwidth.

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Preferably, the analysing means is arranged to analyse phase and amplitude.

If a location of interest is considered, a mathematical modelling operation may be carried out. Thus, the various relevant parameters, such as depth and expected resistivities of the various known strata in the overburden are applied to the mathematical model and the expected results are calculated in dependence upon whether a formation under consideration is oil-bearing or waterbearing. The theoretically predicted results can then be compared with the actual results achieved in the field in order to determine the nature of the formation.

The present invention also extends to a method of surveying subterranean measures which comprises; performing a seismic survey to determine the geological structure of a region; and where that survey reveals the presence of a subterranean reservoir, subsequently performing a method as described above.

The invention may be carried into practice in various ways and some embodiments will now be described by way of example with reference to the accompanying drawings, in which:-

Figure 1 is a schematic section of a system in accordance with the invention.

Figure 1 shows a section through a region which has already been the subject of a seismic survey. The geological structure is known and consists of several strata which form an overburden 11 above a reservoir layer 12 and underlying strata 13. The top of the overburden is a seabed 14 above which is, of course, sea water 15.

In order to determine whether or not the reservoir layer 12 is hydrocarbon-bearing, an electromagnetic surveying technique is carried out. A vessel 16 lays a

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cable 17 on the seabed 14. The cable 17 includes an electromagnetic transmitter 18 and several receivers in the form of dipole antennae, three of which 21, 22, 23 are shown.

The thickness s of the overburden 11 is known to be 1000 m. The depth of the water is about 800 m, though this is of no particular significance. Under these circumstances, the distance 1 between the transmitter 18 and the middle antenna 22 is arranged to be 2000 m, i.e. 2s. The distance between adjacent antennae is about 100 m. In all, the length of the cable 17 is likely be about 4000 m.

When the cable 17 is in position on the seabed 14, the transmitter 18 is activated and transmits an 15 electromagnetic field in the form of a wave. transmission frequency is in the range of about 1 to 30 Hz and the specific value is selected to produce a wavelength λ in the overburden which is approximately equal to s, that is to say, $\lambda \cong 1000 \text{ m}$. The transmitter 18 is tuned 20 for optimum transmission and the antennae 21-23 are tuned to receive transmissions at λ = 1000 m. The antennae 21-23 receive a direct wave 24 from the transmitter and also respective reflected waves 25, 26, 27 which are reflected by the reservoir layer 12 if the layer 12 is hydrocarbon-25 bearing. The received direct wave 24 and received reflected waves 25-27 are analysed and compared with for example the results of forward modelling calculations based on the seismics and typical overburden electrical characteristics and from the results, a judgement can be 30 made as to the nature of the layer 12.

Typically, a frequency of 20 Hz might be selected initially. This would result in a wavelength of 400 m in the sea water and a wavelength of about 1000 m in the

overburden. The wavelength in the layer 12, if hydrocarbon-bearing would be about $5000\ m$. Under these circumstances, the attenuation would be:

5 <u>Direct Wave</u>

Antenna loss -40dB Propagation loss -110dB

Reflected Wave

10 Antenna loss -40dB
Propagation loss -150dB
Reflection loss -20dB

The demanded dynamic range of the receiver system

will then be 210 dB - 150 dB = 60 dB. By appropriate suppression of the direct wave, this demand will decrease dramatically and the resolution of the reflected signal will possibly be increased.

The transmission would be carried out for several minutes at a continuous power level of perhaps 10 kw.

This procedure is then repeated at a different frequency. This would result in different wavelengths and possibly consequent re-tuning of the antennae system. At a frequency of for example 5Hz, the wavelength in sea water would be 800 m and the wavelength in the overburden, about 2000 m. The wavelength in the layer 12, if hydrocarbon-bearing, would be 10 km. The attenuation would be:

30 <u>Direct Wave</u>

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Antenna loss -40dB Propagation loss -55dB

Reflected Wave

Antenna loss -40dB Propagation loss -75dB

Reflection loss -30dB

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The demand for dynamic range of receiver system is now 145 dB - 95 dB = 50 dB.

In a preferred regime, the frequency would be increased stepwise over a range, for example 5 to 20 Hz.

The entire procedure can then be repeated in different locations and at different orientations. It will also be appreciated that by repeating the procedure after a period of production, the change in condition of a reservoir can be determined. This can be of value in assessing the positions in a particular field where hydrocarbons might still be present, and where the well might be depleted.

Claims:

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- 1. A method of determining the nature of a submarine or subterranean reservoir whose approximate geometry and location are known, which comprises: applying a time varying electromagnetic field to the strata containing the reservoir; detecting the electromagnetic wave field response; and analysing the effects on the characteristics of the detected field that have been caused by the reservoir, thereby determining the content of the reservoir, based on the analysis.
 - 2. A method as claimed in Claim 1, in which the field is applied using one or more stationary transmitters located on the earth's surface.
- 3. A method as claimed in Claim 1 or Claim 2, in which the detection is carried out by one or more stationary receivers located on the earth's surface.
- 4. A method as claimed in Claim 2 or Claim 3, in which the transmitter and/or receivers are located on or close to the seabed or the bed of some other area of water.
- 5. A method as claimed in any preceding Claim, in which the transmitted field is in the form of a wave.
 - 6. A method as claimed in any preceding Claim, in which the field is transmitted for a period of time from 30 seconds to 60 minutes.
 - 7. A method as claimed in Claim 6, in which the transmission time is from 3 minutes to 30 minutes.

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- 8. A method as claimed in any of Claims 3 to 7, in which the receivers are arranged to detect a direct wave and a wave reflected from the reservoir, and the analysis includes extracting phase and amplitude data of the reflected wave from corresponding data from the direct wave.
- 9. A method as claimed in any of Claims 5 to 8, in which the wavelength of the transmission is given by the formula

 $0.1s \leq \lambda \leq 10s$;

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- where λ is the wavelength of the transmission through the overburden and s is the distance from the seabed to the reservoir.
- 10. A method as claimed in any of Claims 5 to 9, in which distance between the transmitter and a receiver is given20 by the formula

0.5 $\lambda \leq 1 \leq 10 \lambda$;

- where λ is the wavelength of the transmission through the overburden and 1 is the distance between the transmitter and the receiver.
 - 11. A method as claimed in Claims 9 and 10, in which, substantially,

 $1 = 2s = 2\lambda.$

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12. A method as claimed in any of Claims 3 to 11, in which the transmission frequency is from 0.1 Hz to 1 kHz.

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13. A method as claimed in Claim 12, in which the transmission frequency is from 1 to 50 Hz.

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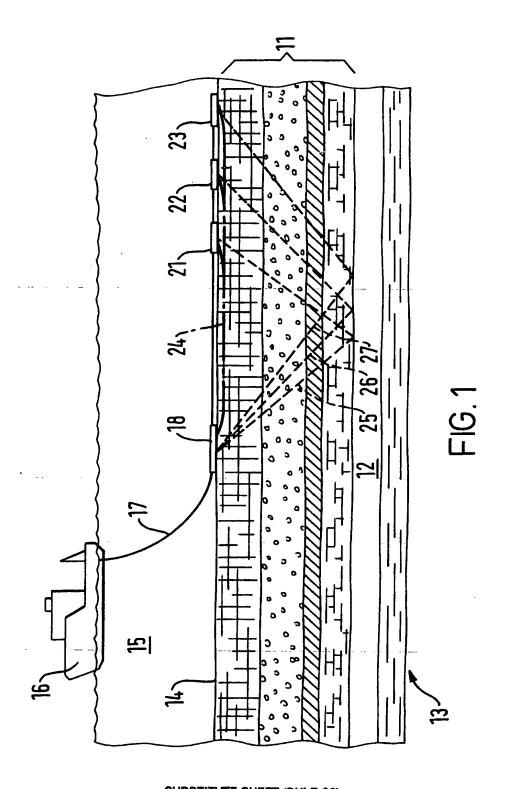
14. A method as claimed in any of Claims 3 to 13, in which a first transmission is made at a first frequency and received by each receiver in a tuned array of receivers, then a second transmission is made at a second frequency and received by the same tune array of receivers, the receivers being tuned to receive their respective transmission, the transmitter(s) also being tuned for optimum transmission.

15. A method as claimed in any preceding Claim, in which the analysis includes comparing the results of the measurements taken with the results of a mathematical simulation model based on the known properties of the reservoir and overburden conditions.

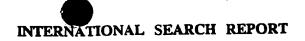
- 16. A method as claimed in any of Claims 8 to 15, which includes suppressing the direct wave, thereby reducing the required dynamic range of the receivers and increasing the resolution of the reflected wave.
- 17. Apparatus for determining the nature of a subterranean reservoir whose approximate geometry and location are known comprising: means for applying a time varying electromagnetic field to the strata containing the reservoir; means for detecting the electromagnetic wave field response, and means for analysing the effects on the detected field that have been caused by the reservoir, thereby enabling the content of the reservoir to be

determined based on the analysis.

- 18. Apparatus as claimed in Claim 17, in which the means for applying the field comprises a transmitter and the means for detecting the field comprises an array of receivers.
- 19. Apparatus as claimed in Claim 18, in which the transmitter and the receivers comprise dipole antennae or 10 coils.
 - 20. Apparatus as claimed in any of Claims 17 to 19, in which there are more than one transmitter.
- 15 21. Apparatus as claimed in any of Claims 17 to 20, in which the analysing means is arranged to analyse phase and amplitude.
- 22. A method of surveying subterranean measures which comprises; performing a seismic survey to determine the geological structure of a region; and where that survey reveals the presence of a subterranean reservoir, subsequently performing a method as claimed in any of Claims 1 to 16 to determine the nature of the reservoir.



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A. CLASSIFICATION OF SUBJECT MATTER IPC 7 G01V3/12 G01V11/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

Category *	Citation of document, with Indication, where appropriate, of the relevant passages	Relevant to claim No.
Υ	WO 98 28638 A (KARTASHOV MIKHAIL VIKTOROVICH ; NIZAMOV ALEXANDR ZHAKFEROVICH (RU);) 2 July 1998 (1998-07-02) abstract	1-3,5, 12-14, 17-22
Y	US 4 633 182 A (DZWINEL JAN) 30 December 1986 (1986-12-30) column 2, line 33 -column 3, line 55 column 6, line 44 - line 53	1-3,5, 12-14, 17-22
A	FR 2 479 992 A (DUROUX JEAN) 9 October 1981 (1981-10-09) page 2, line 7 -page 5, line 35	1-5,8, 12-14, 16,17, 19-21
	-/	

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		PCT/GB 99/02823			
	ation) DOCUMENTS CONSIDERED TO BE RELEVANT		Relevant to claim No.		
Category °	Citation of document, with indication, where appropriate, of the relevant passages		Netevant to claim 140.		
Α	US 5 563 513 A (TASCI M TAHSIN ET AL) 8 October 1996 (1996-10-08) column 2, line 20 - line 63		1,17,22		
A	GREAVES R J ET AL: "NEW DIMENSIONS IN GEOPHYSICS FOR RESERVOIR MONITORING" SPE FORMATION EVALUATION, US, THE SOCIETY, RICHARDSON, TX, vol. 6, no. 2, page 141-150 XP000646267 ISSN: 0885-923X page 148		1,17		
			• •		
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information on patent family members

Inter and Application No PCT/GB 99/02823

Patent document cited in search report		Patent family member(s)		Publication date	
A	02-07-1998	RU AU	2100829 C 2183097 A	27-12-1997 17-07-1997	
Α	30-12-1986	CA DE FR YU	1214519 A 3400284 A 2542097 A 24584 A	25-11-1986 06-09-1984 07-09-1984 31-10-1987	
Α	09-10-1981	NONE			
Α	08-10-1996	AU CA WO	1397595 A 2178315 A 9516212 A	27-06-1995 15-06-1995 15-06-1995	
	A A	A 02-07-1998 A 30-12-1986 A 09-10-1981	A 02-07-1998 RU AU A 30-12-1986 CA DE FR YU A 09-10-1981 NONE A 08-10-1996 AU CA	A 02-07-1998 RU 2100829 C AU 2183097 A A 30-12-1986 CA 1214519 A DE 3400284 A FR 2542097 A YU 24584 A A 09-10-1981 NONE A 08-10-1996 AU 1397595 A CA 2178315 A	